

Capitolul 5

Etaje de iesire

5.1. Notiuni generale

5.1. Caracteristici generale

- debiteaza putere intr-o sarcina, avand un randament ridicat si putere disipata redusa pe tranzistoarele finale
- impedanta redusa de iesire
- excursie maxima a tensiunii de iesire
- distorsiuni minime

Clasa A:

- distorsiuni foarte reduse
- randament redus

Clasa B:

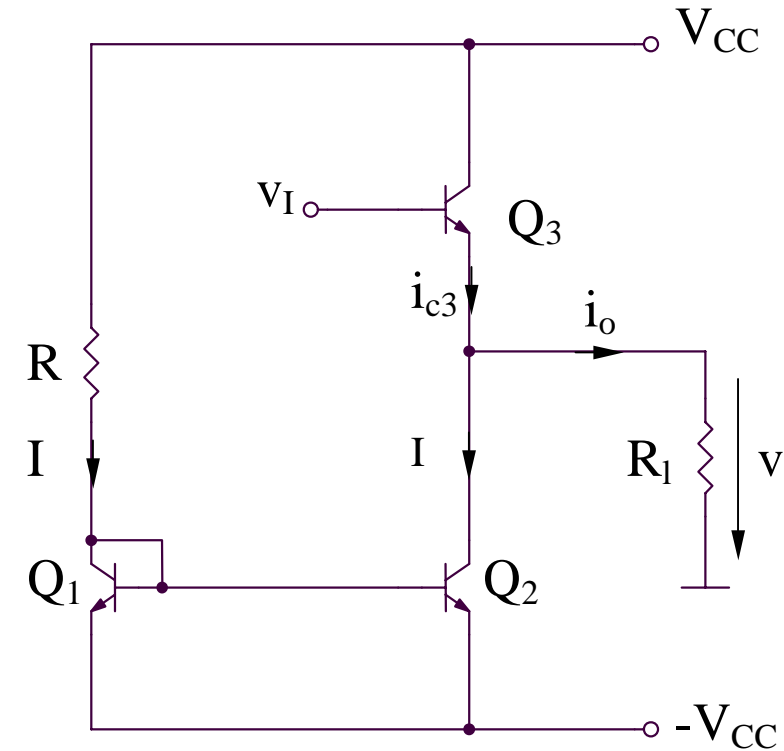
- distorsiuni importante
- randament foarte bun

Clasa AB:

- distorsiuni reduse
- randament bun

5.2. Etajul de iesire in clasa A, configuratie colector comun

5.2. Etajul de iesire in clasa A, configuratie colector comun



In repaus:

$$v_O = 0; i_O = 0$$

$$I_{C3} = I; V_{CE3} = V_{CC}$$

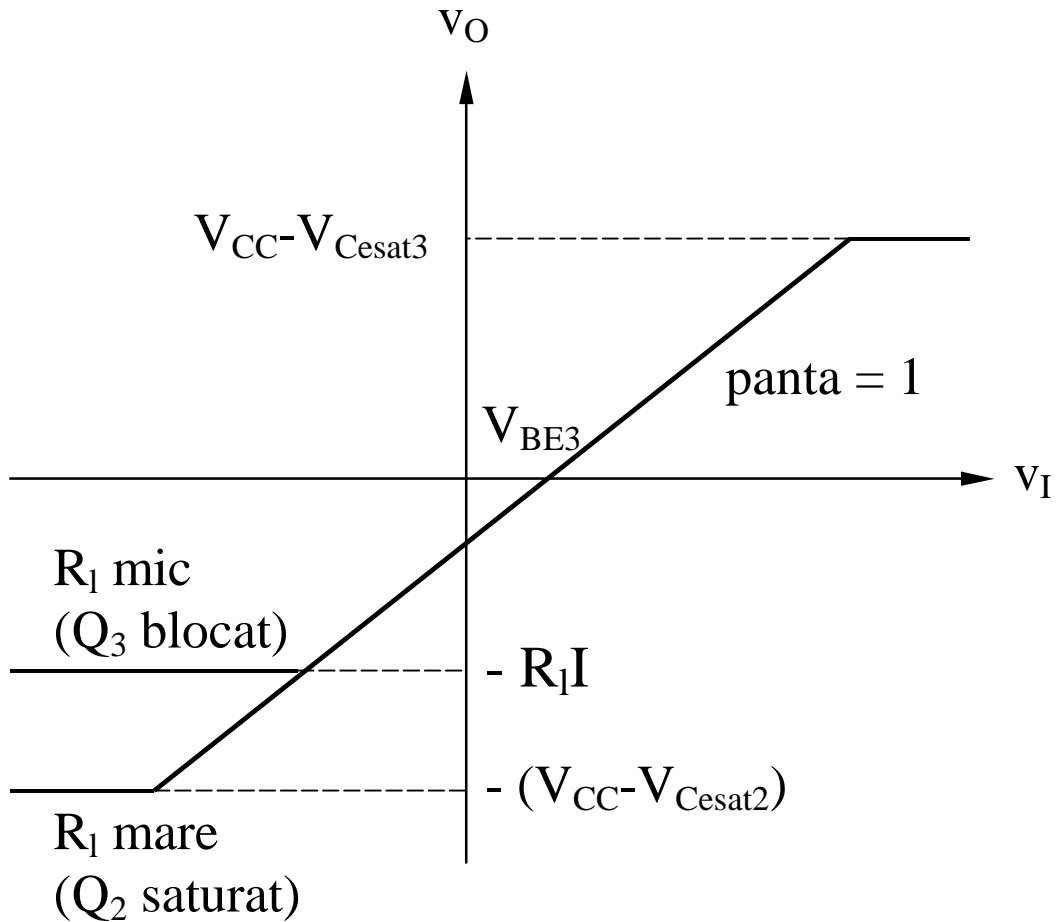
$$V_I = V_{BE3} = V_{th} \ln\left(\frac{I}{I_S}\right)$$

Caracteristica de transfer $v_O = f(v_I)$

$$\left. \begin{aligned} v_I &= v_{BE3} + v_O \\ v_{BE3} &= V_{th} \ln\left(\frac{i_{c3}}{I_S}\right) \\ i_{c3} &= I + \frac{v_O}{R_L} \end{aligned} \right\} \Rightarrow v_I = v_O + V_{th} \ln\left(\frac{I + \frac{v_O}{R_L}}{I_S}\right)$$

Cu $\frac{v_O}{R_L} \ll I$, $V_{th} \ln\left(\frac{I}{I_S}\right) = V_{BE3}$, expresia caracteristici de transfer

devine, in consecinta $v_I = v_O + v_{BE3}$, deci liniara.



$$i_{C3} = I + \frac{v_O}{R_1}$$

$$i_{C3} = I + \frac{V_{CC} - v_{CE3}}{R_1}$$

$$i_{C3} = 0 \Rightarrow v_{CE3} = V_{CC} + IR_1$$

Valoarea maxima pozitiva a tensiunii de iesire este:

$$V_{OM}^+ = V_{CC} - V_{CEsat3}$$

Valoarea maxima negativa a tensiunii de iesire depinde de valoarea R_1 :

- pentru valori mari ale R_1 , limita negativa a tensiunii de iesire este data de saturatia tranzistorului Q_2

$$/V_{OM}^- / = V_{CC} - V_{CEsat2}$$

- pentru valori mici ale R_1 , limita negativa a tensiunii de iesire este data de blocarea tranzistorului Q_2

$$/V_{OM}^- / = IR_l < V_{CC} - V_{CEsat2}$$

Relatii energetice fundamentale

Notand:

$$\hat{V}_O = KV_{CC}$$

K fiind factorul de utilizare a tensiunii de alimentare, $0 \leq K < 1$. Deci:

$$\hat{I}_O = \frac{\hat{V}_O}{R_l} = \frac{KV_{CC}}{R_l} = KI$$

Puterea disipata pe tranzistorul Q_3 este:

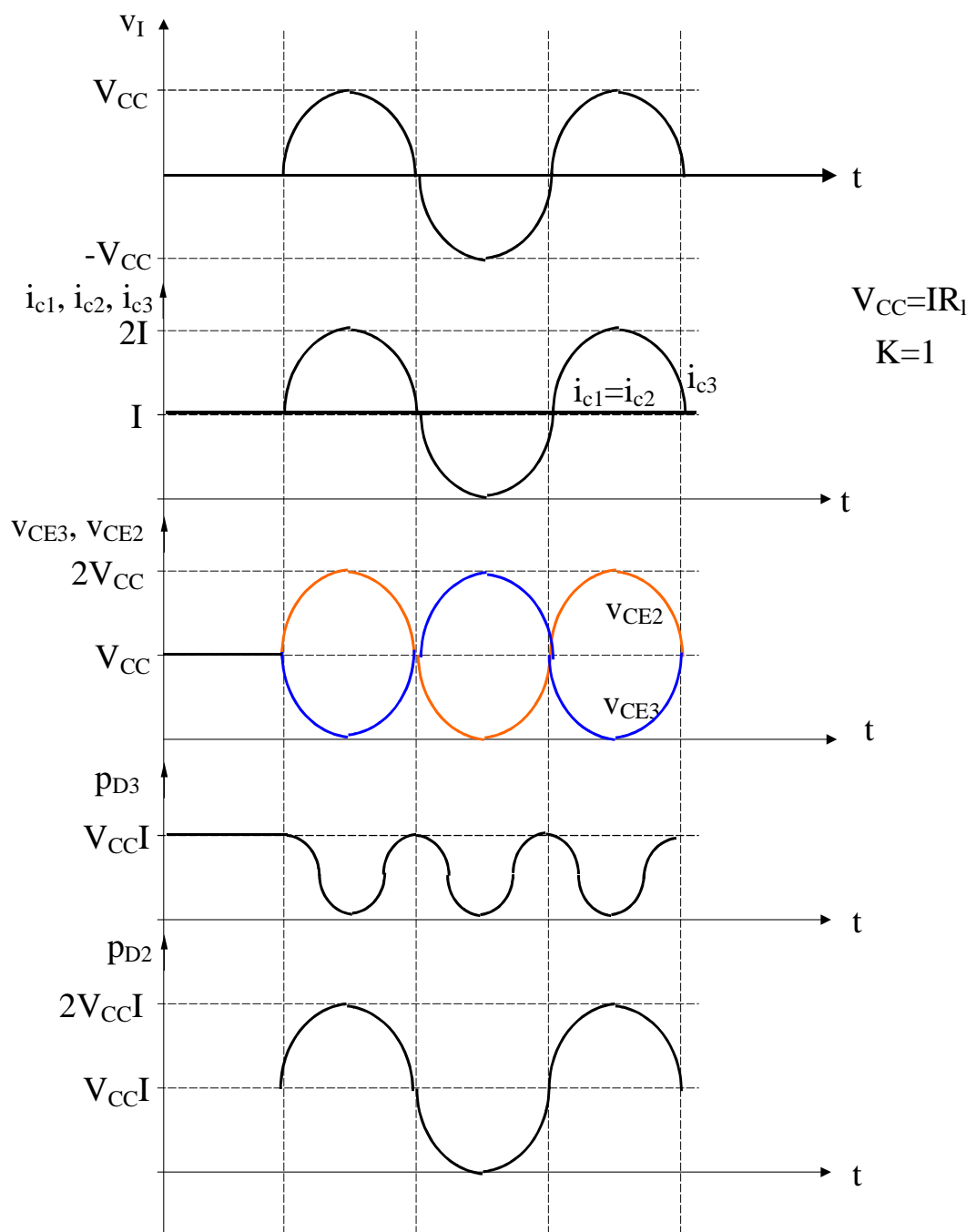
$$p_{D3} = v_{CE3}i_{C3} = \left(V_{CC} - \hat{V}_O \sin \omega t \right) \left(I + I_O \hat{\sin} \omega t \right)$$

$$p_{D3} = V_{CC}I(1 - K \sin \omega t)(1 + K \sin \omega t)$$

$$p_{D3} = V_{CC}I(1 - K^2 \sin^2 \omega t) = V_{CC}I \left(1 - \frac{K^2}{2} + \frac{K^2}{2} \cos 2\omega t \right)$$

Deci, puterea medie disipata pe tranzistorul Q_3 va fi:

$$P_{D3} = \frac{1}{2\pi} \int_0^{2\pi} p_{D3} d\omega t = V_{CC}I \left(1 - \frac{K^2}{2} \right)$$



Puterea disipata pe tranzistorul Q_2 este:

$$P_{D2} = i_{C2} v_{CE2} = I \left(V_{CC} + \hat{V}_O \sin \omega t \right) = I V_{CC} (1 + K \sin \omega t)$$

Deci, puterea medie disipata pe tranzistorul Q_2 va fi

$$P_{D2} = \frac{1}{2\pi} \int_0^{2\pi} p_{D2} d\omega t = V_{CC} I$$

Puterea consumata din sursele de alimentare va avea expresia:

$$P_A = V_{CC} i_{C3} + V_{CC} i_{C2} = V_{CC} (2I + KI \sin \omega t)$$

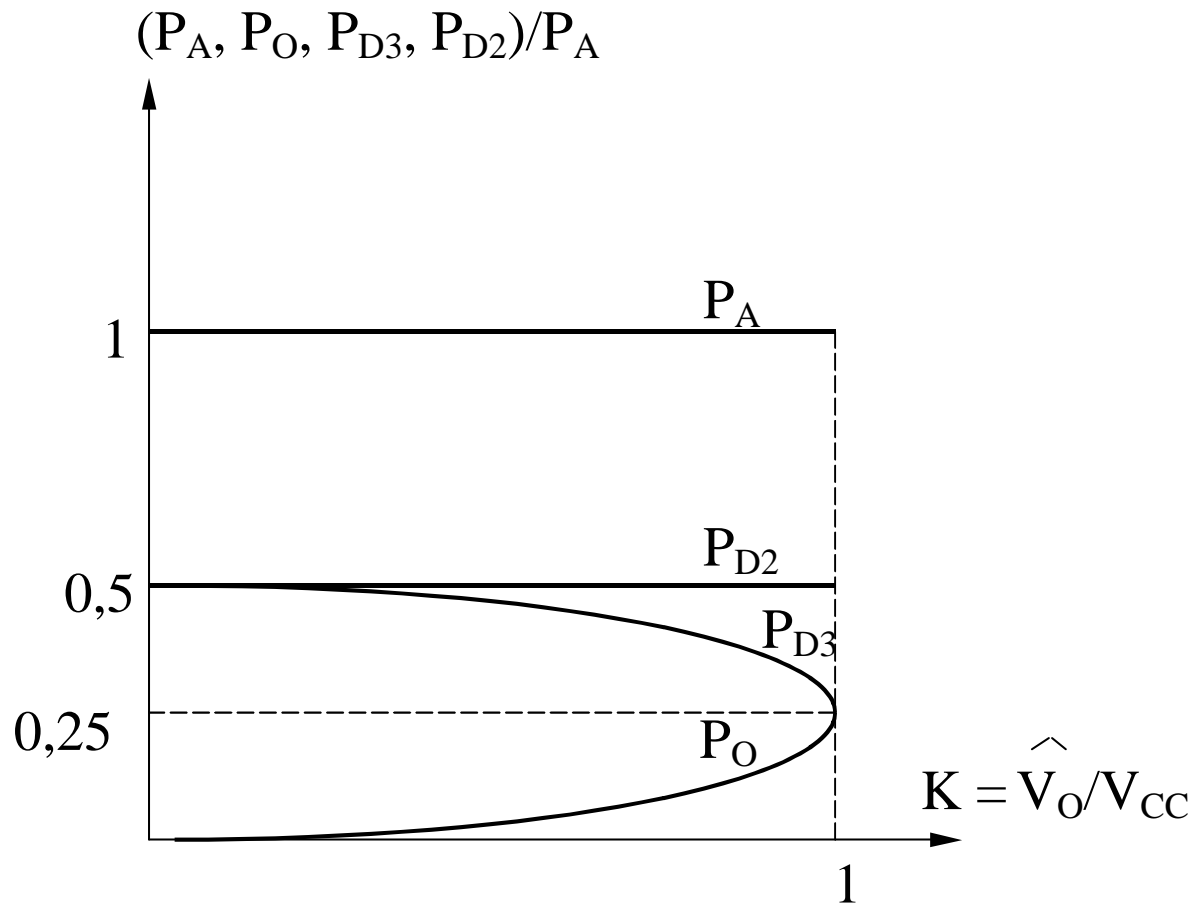
$$P_A = \frac{1}{2\pi} \int_0^{2\pi} p_A d\omega t = 2V_{CC} I$$

Puterea medie la iesire este:

$$P_O = \frac{1}{2\pi} \int_0^{2\pi} p_O d\omega t = \frac{1}{2\pi} \int_0^{2\pi} (KV_{CC} \sin \omega t)(KI \sin \omega t) d\omega t = \frac{K^2 V_{CC} I}{2}$$

$$\eta_A = \frac{P_O}{P_A} = 25\% K^2$$

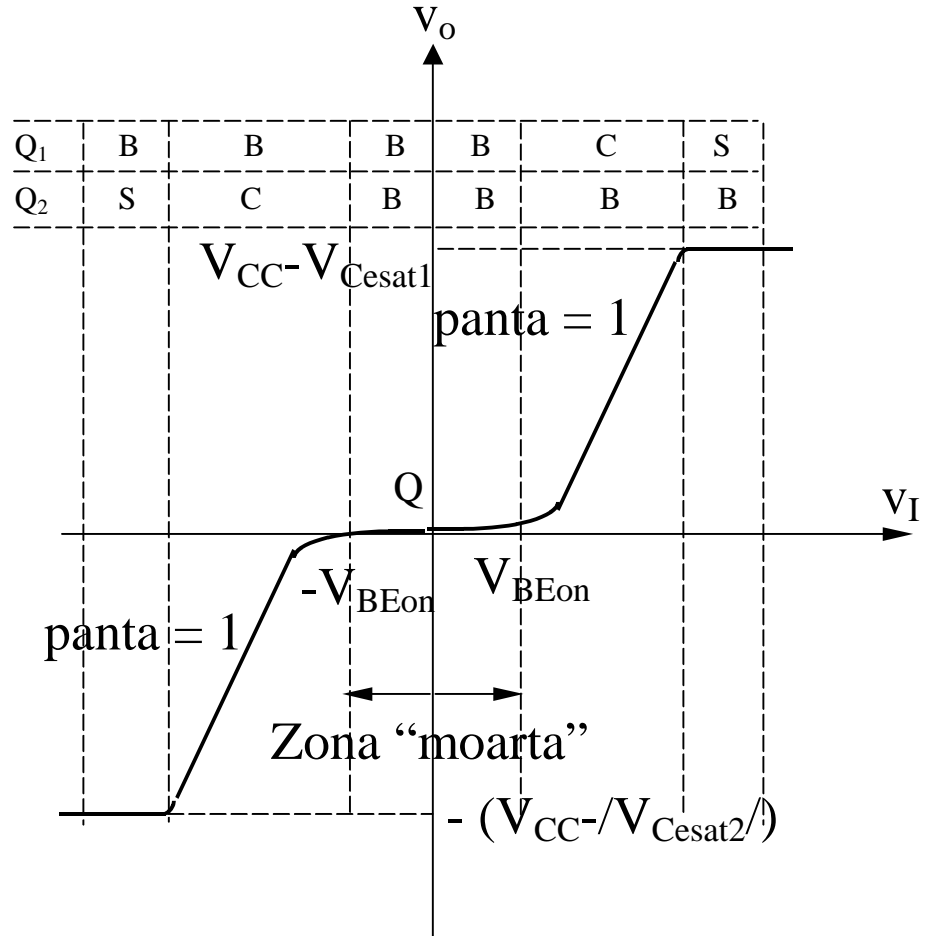
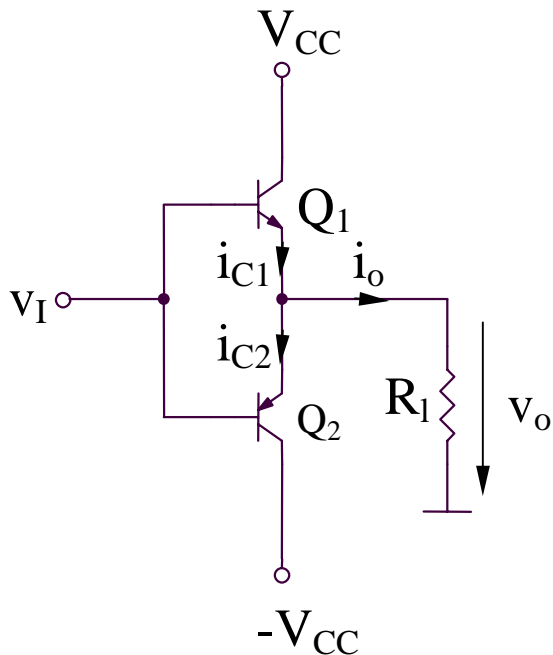
avand o valoare maxima de 25%.



$$P_{D2} = P_{D3} + P_O$$

$$P_A = P_{D2} + P_{D3} + P_O = 2P_{D2}$$

5.3. Etajul de iesire elementar in clasa B

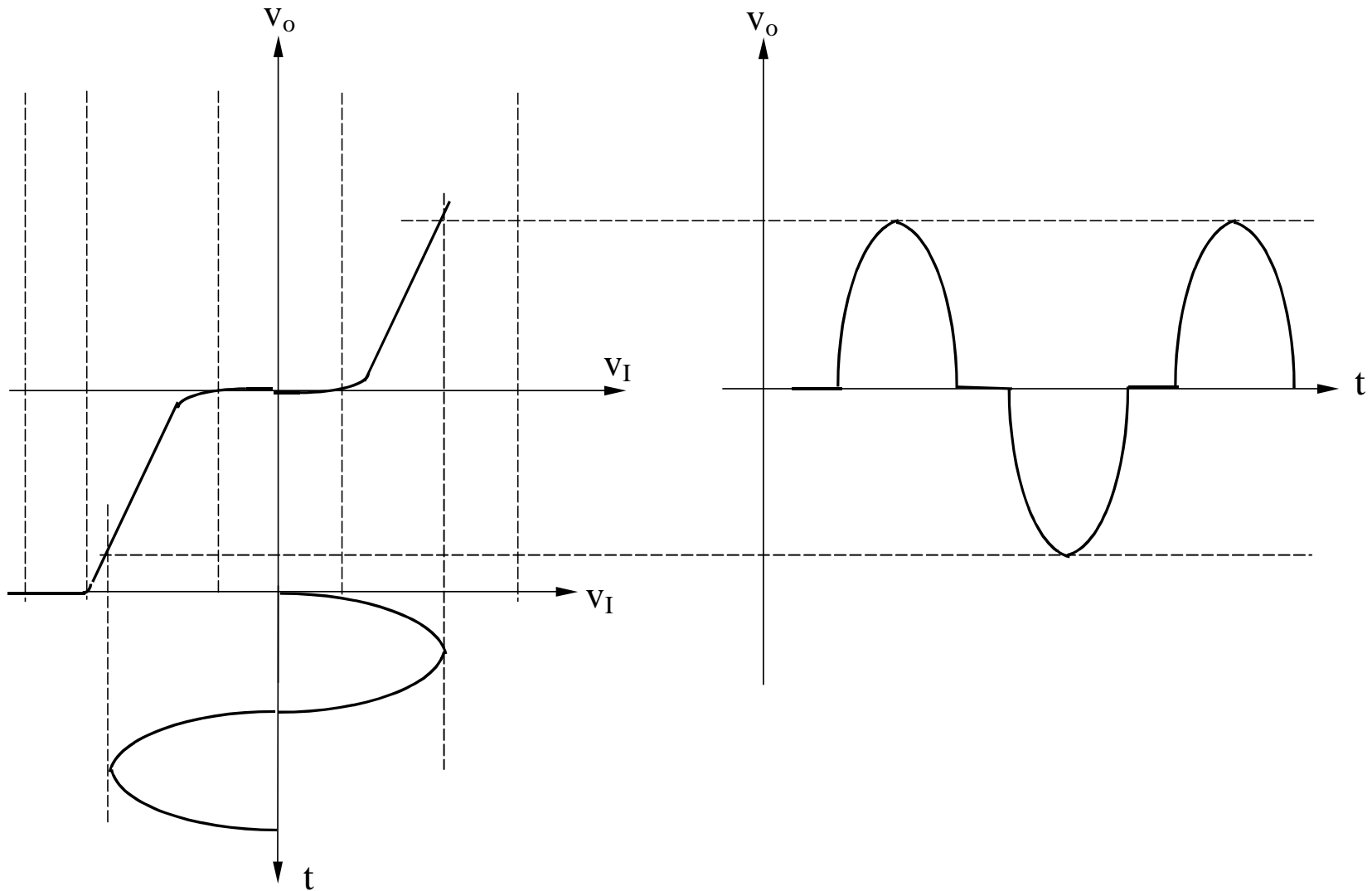


In repaus:

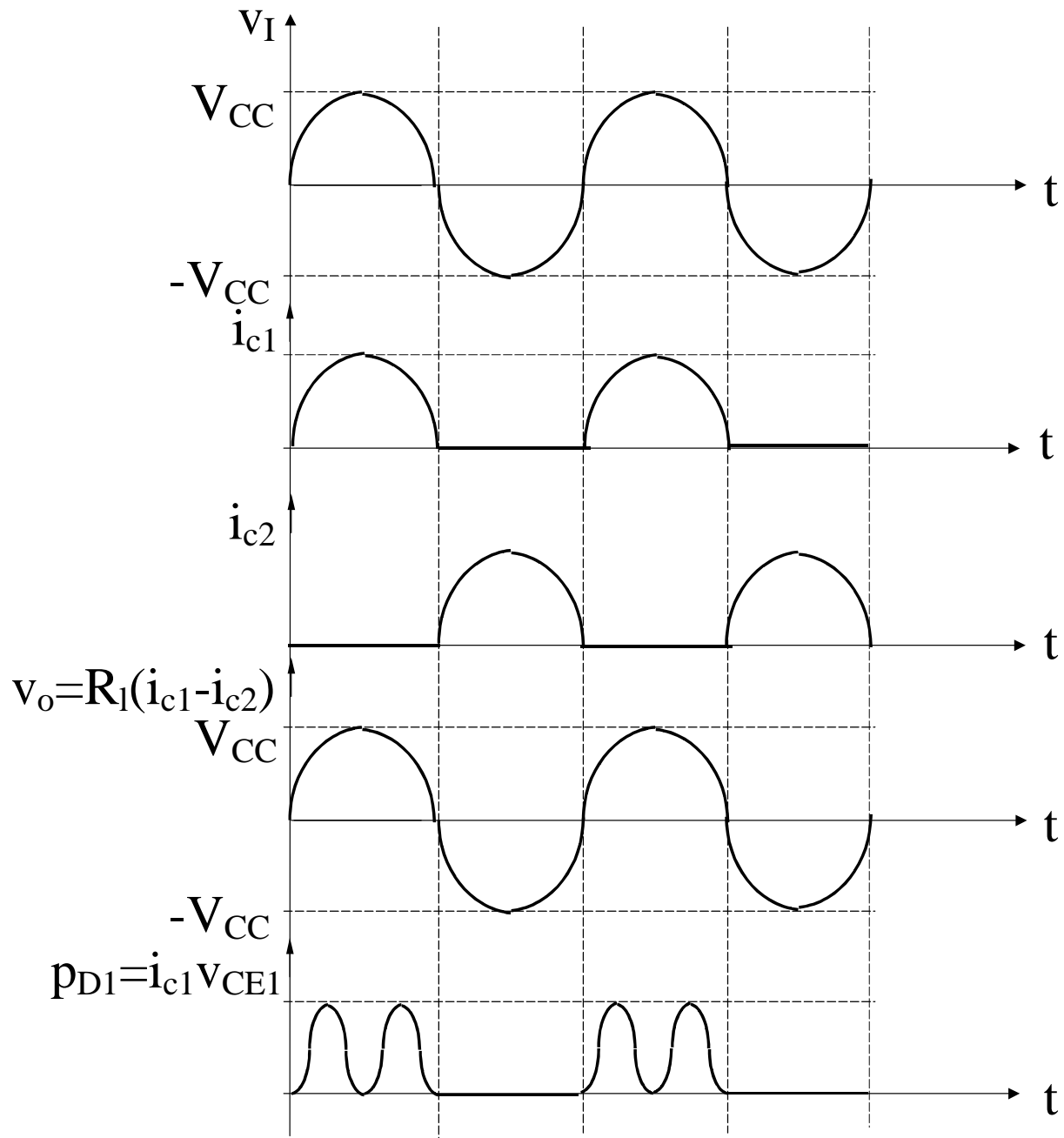
$$v_O = 0; i_O = 0; i_{c1} = i_{c2} = I; v_{BE1} + v_{EB2} = 0$$

Daca:

$$Q_1 \equiv Q_2; I_{S1} = I_{S2} = I_S \Rightarrow 2V_{th} \ln\left(\frac{I}{I_S} + 1\right) = 0 \Rightarrow I = 0 \Rightarrow i_{c1} = i_{c2} = 0$$



Característica de transfer



Dezavantajul major al etajelor de iesire in clasa B
- “zona moarta” (distorsiuni)

Solutie:

- utilizarea etajelor de iesire in clasa AB

Relatii energetice fundamentale

Notand:

$$\hat{V}_O = KV_{CC}$$

K fiind factorul de utilizare a tensiunii de alimentare, $0 \leq K < 1$.

Puterea medie la iesire, P_O , este:

$$P_O = \frac{1}{2\pi} \int_0^{2\pi} p_O d\omega t = \frac{1}{2\pi} \int_0^{2\pi} (KV_{CC} \sin \omega t) \left(K \frac{V_{CC}}{R_l} \sin \omega t \right) d\omega t = \frac{K^2 V_{CC}^2}{2R_l}$$

Notand cu P_A puterea totala consumata de ambele surse de tensiune de alimentare:

$$P_A = 2V_{CC}I_{CC}$$

Componenta continua I_{CC} fiind:

$$I_{CC} = \frac{1}{2\pi} \int_0^\pi I_C \sin \omega t d\omega t = \frac{1}{\pi} \hat{I}_C = \frac{1}{\pi} \frac{\hat{V}_O}{R_l} = \frac{KV_{CC}}{\pi R_l}$$

se obtine:

$$P_A = K \frac{2V_{CC}^2}{\pi R_l}$$

Puterea disipata medie P_D pentru o pereche de tranzistoare in clasa B este:

$$P_D = P_A - P_O = \frac{V_{CC}^2}{2R_l} \left(\frac{4K}{\pi} - K^2 \right)$$

Relatia anterioara reprezinta o parabola in K, al carei maxim se poate obtine prin anularea derivatei:

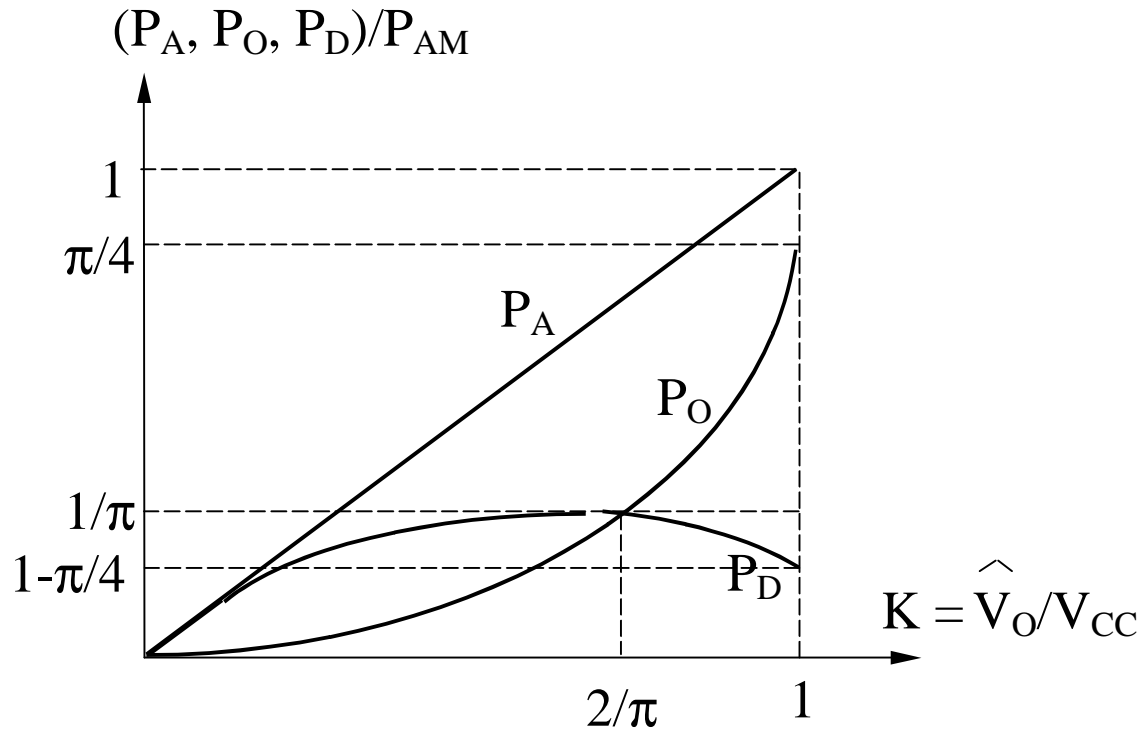
$$\frac{4}{\pi} - 2K = 0 \Rightarrow K = \frac{2}{\pi}$$

Pentru aceasta valoare a lui K se va obtine maximul puterii medii disipate (pentru amandoua tranzistoarele):

$$P_{DM} = \frac{2}{\pi^2} \frac{V_{CC}^2}{R_l} = \frac{4}{\pi^2} \frac{V_{CC}^2}{2R_l} = \frac{4}{\pi^2} P_{OM} \qquad P_{OM} = \frac{V_{CC}^2}{2R_l}$$

Pe graficele urmatoare sunt reprezentate puterile normate in functie de K:

$$\frac{P_A}{P_{AM}} = K; \quad \frac{P_O}{P_{AM}} = \frac{\pi K^2}{4}; \quad \frac{P_D}{P_{AM}} = K \left(1 - \frac{K\pi}{4} \right)$$

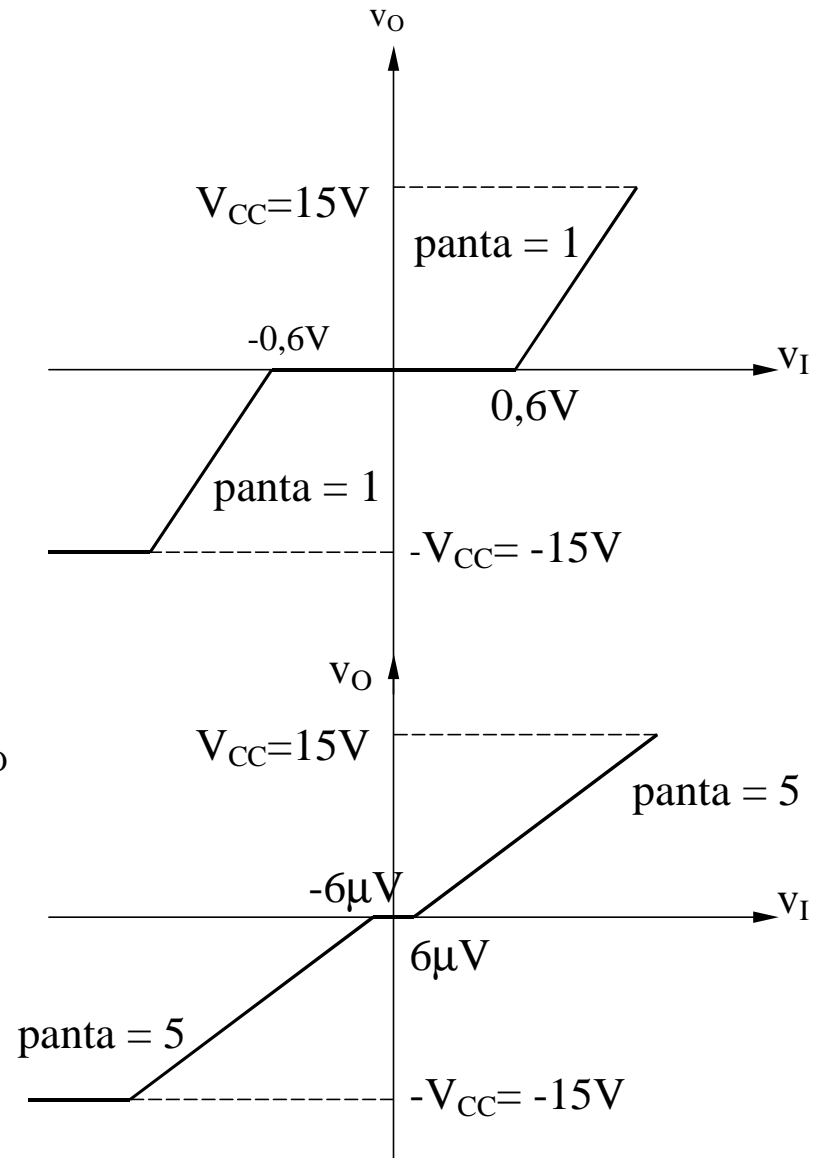
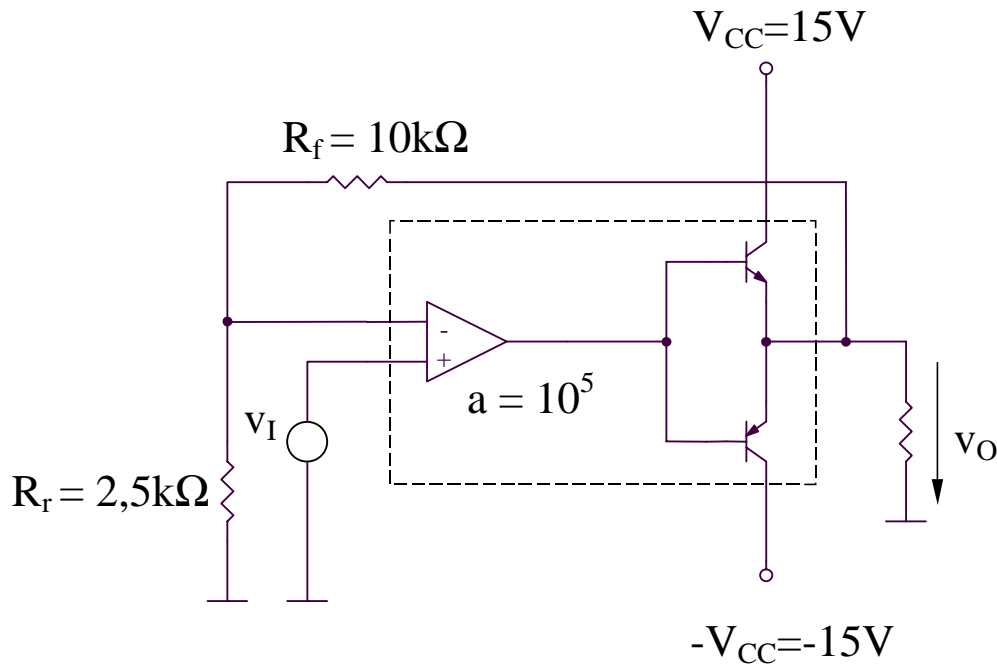


Randamentul etajului este:

$$\eta = \frac{P_O}{P_A} = K \frac{\pi}{4}$$

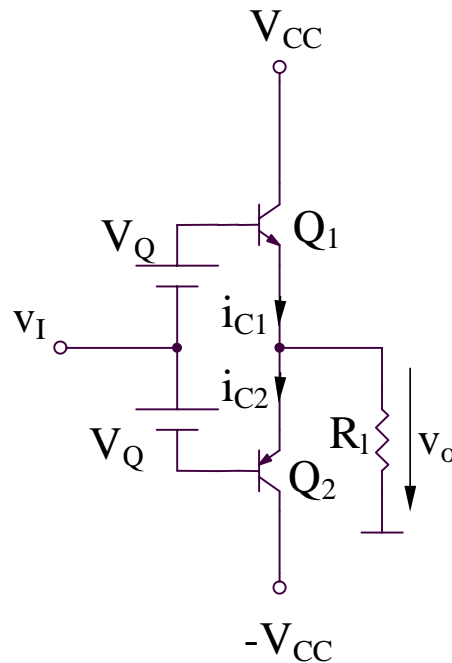
Valoarea sa maxima se obtine pentru $K=1$ si este $\pi/4$ (78.5%).

5.4. Reducerea neliniaritatii etajului de iesire in clasa B prin utilizarea rectiei negative



5.5. Etajul de iesire in clasa AB

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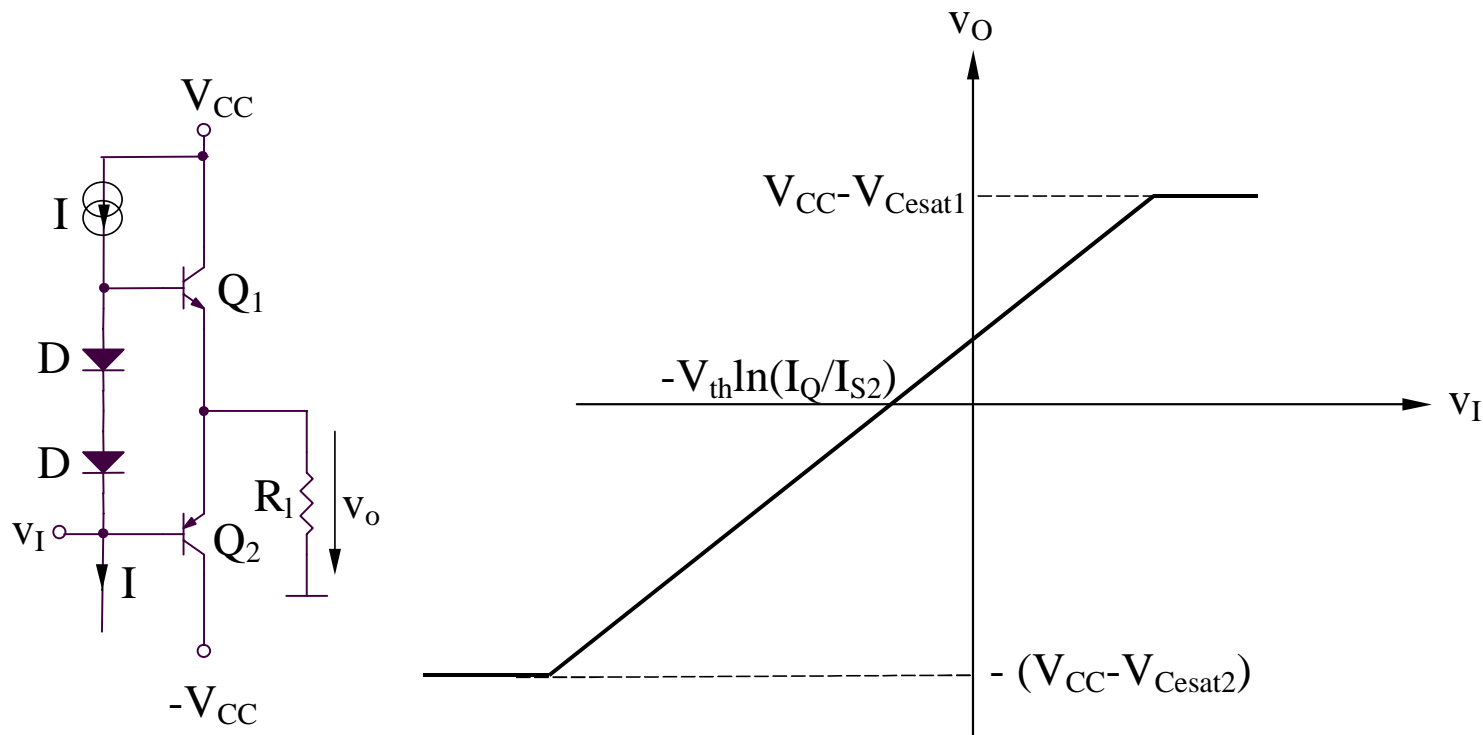


Pentru obtinerea unei bune liniaritati a functiei de transfer, este necesar:

- sa existe o imperechere cat mai buna intre parametrii tranzistoarelor complementare
- sa se realizeze o pre-polarizare corespunzatoare a etajului de iesire in repaus
- pre-polarizarea implementata sa asigure evitarea ambalarii termice a etajului

Circuit pentru evitarea ambalarii termice a etajului de iesire (1)

Tensiunea care asigura pre-polarizarea etajului de iesire trebuie sa prezinte o variatie particulara cu temperatura (de exemplu, o tensiune baza-emitor)

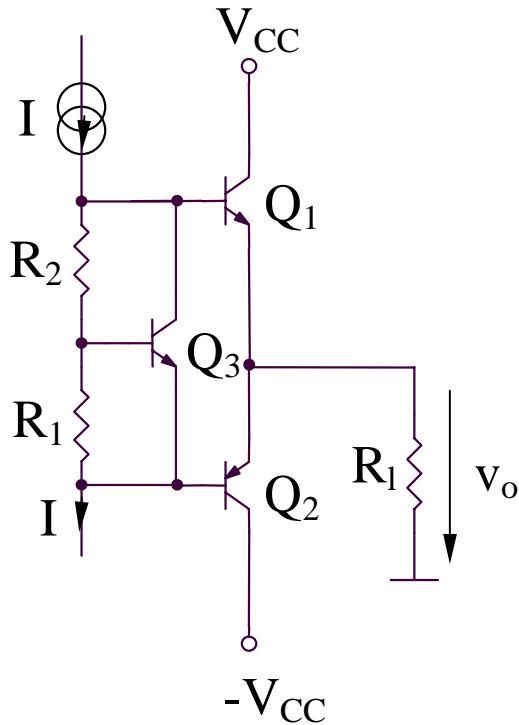


Tranzistoarele conectate ca diode trebuie sa prezinte o dependenta de temperatura similara cu cea a tranzistoarelor finale. In repaus:

$$v_o = 0$$

$$V_{BE1} + V_{EB2} = 2V_D \Rightarrow V_{th} \ln\left(\frac{I_Q}{I_{S1}} \frac{I_Q}{I_{S2}}\right) = 2V_{th} \ln\left(\frac{I}{I_{SD}}\right) \Rightarrow I_Q = I \frac{\sqrt{I_{S1} I_{S2}}}{I_{SD}}$$

Circuit pentru evitarea ambalarii termice a etajului de iesire (2)

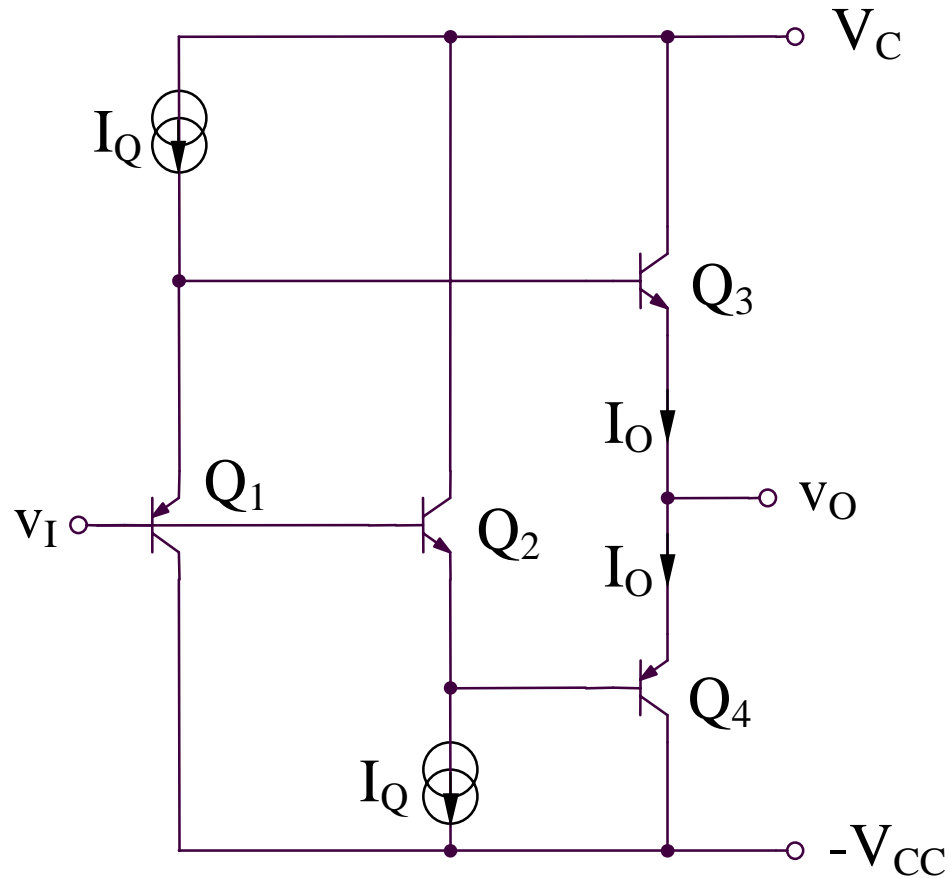


$$\left. \begin{aligned} v_{BE1} + v_{EB2} &= v_{CE3} \\ v_{CE3} &= \frac{v_{BE3}}{R_1} (R_1 + R_2) \end{aligned} \right\} \Rightarrow$$

$$\Rightarrow V_{th} \left(\ln \frac{I_Q}{I_{S1}} + \ln \frac{I_Q}{I_{S2}} \right) = \left(1 + \frac{R_2}{R_1} \right) V_{th} \ln \frac{I}{I_{S3}}$$

$$\Rightarrow I_Q = \sqrt{I_{S1} I_{S2} \left(\frac{I}{I_{S3}} \right)^{1 + \frac{R_2}{R_1}}}$$

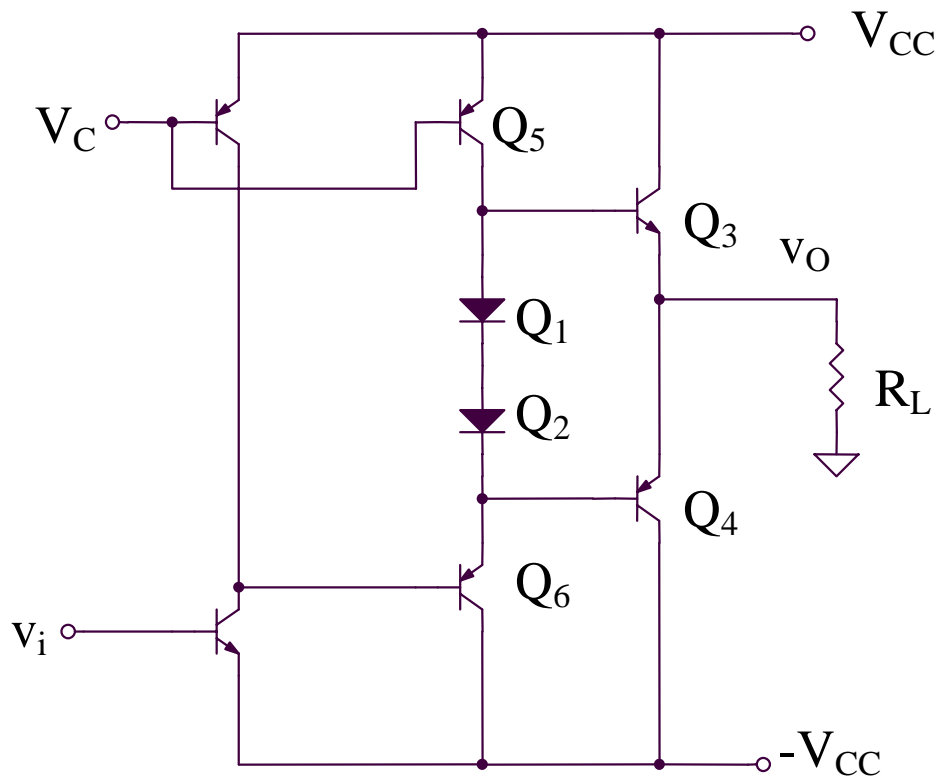
Circuit pentru evitarea ambalarii termice a etajului de iesire (3)



$$|V_{BE1}| + V_{BE2} = V_{BE3} + |V_{BE4}|$$

$$2V_{th} \ln \frac{I_Q}{I_S} = 2V_{th} \ln \frac{I_O}{I_S} \Rightarrow I_O = I_Q$$

Circuit pentru evitarea ambalarii termice a etajului de iesire (4)



$$V_{BE1} + V_{BE2} = V_{BE3} + V_{EB4}$$

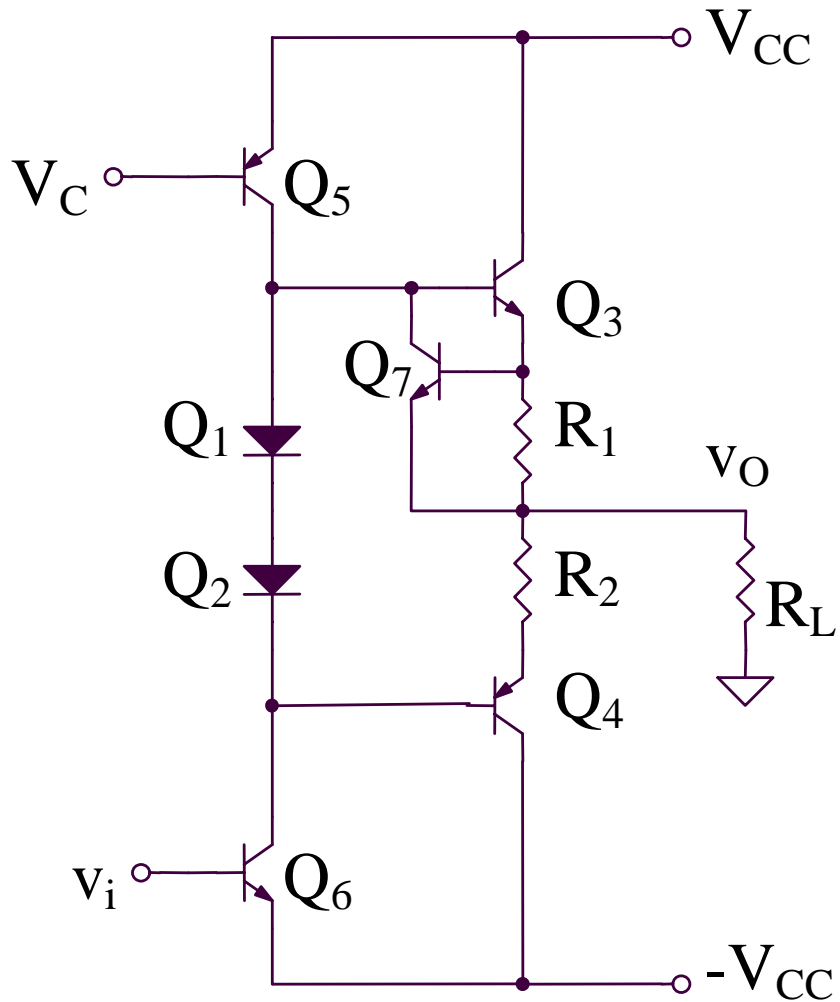
$$V_{th} \ln \frac{I_{C1}}{I_{S1}} + V_{th} \ln \frac{I_{C2}}{I_{S2}} = V_{th} \ln \frac{I_{C3}}{I_{S3}} + V_{th} \ln \frac{I_{C4}}{I_{S4}}$$

$$\Rightarrow I_{C3} = I_{C4} = I_{C1} \sqrt{\frac{I_{S3} I_{S4}}{I_{S1} I_{S2}}}$$

$$V_{O_{max}}^+ = V_{CC} - V_{EC5_{sat}} - V_{BE3}$$

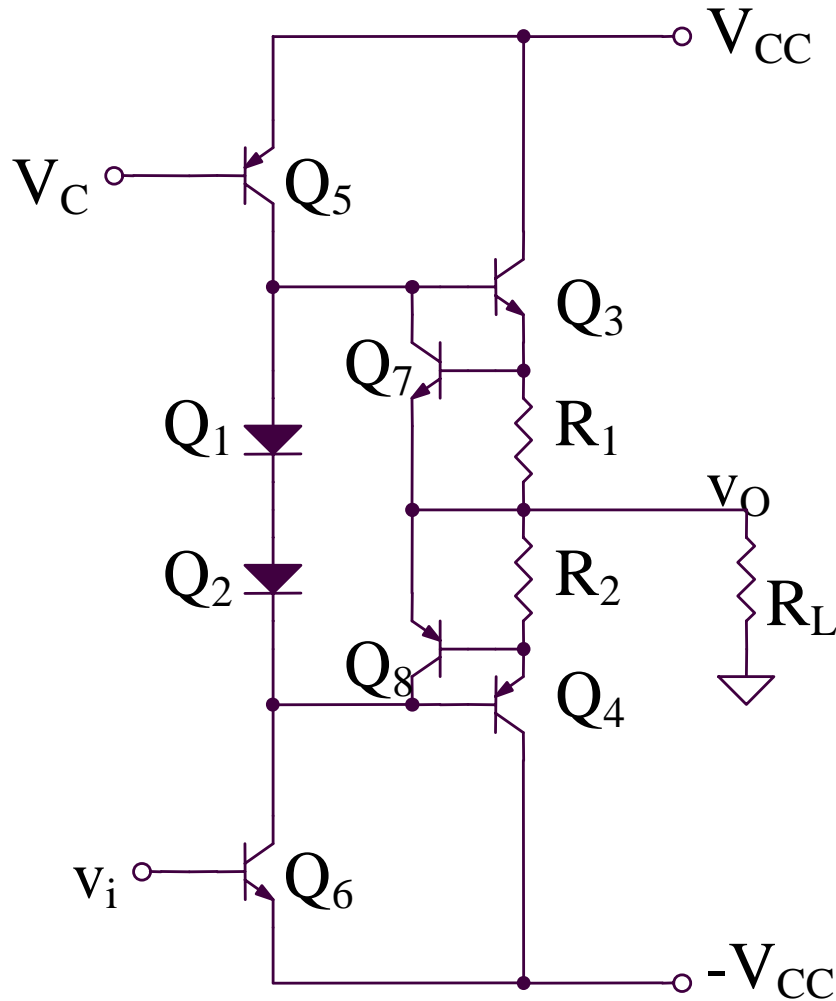
$$V_{O_{max}}^- = -V_{CC} + V_{EC6_{sat}} + V_{EB4}$$

Circuit pentru protectia la suprasarcina (1)



$$I_{Omax}^+ = \frac{V_{BE7}}{R_1}$$

Circuit pentru protectia la suprasarcina (2)



$$I_{O_{max}}^+ = \frac{V_{BE7}}{R_1}$$

$$I_{O_{max}}^- = \frac{V_{EB8}}{R_2}$$